

Features

- I High-Voltage(500V) start up Circuit
- I Current Mode Control
- I Programmable Switching Frequency
- I Internal Slope Compensation
- I Under Voltage Lockout(UVLO)
- I Over Voltage Protection (OVP)
- I Over Load Protection(OLP)
- I Leading _Edge Blanking

Applications

- I AC/DC Adapter
- I Open Frame Switching Power Supply
- I LCD Monitor/TV Power

General Description

The PR8275 is a current-mode PWM controller with excellent power-saving operation. It provides a high voltage current source to directly supply the startup current from bulk capacitor and further to provide a lossless startup circuit. The integrated functions such as the leading-edge blanking of the current sensing, internal slope compensation, and the small package provide the users a high efficiency, minimum

external component counts, and low cost solution for AC/DC power applications. Furthermore, the embedded over voltage protection, over load protection and the special green-mode control provide the solution for users to design a high performance power circuit easily. The PR8275 is offered in both SOP-8 and DIP-8 package.

Typical Application

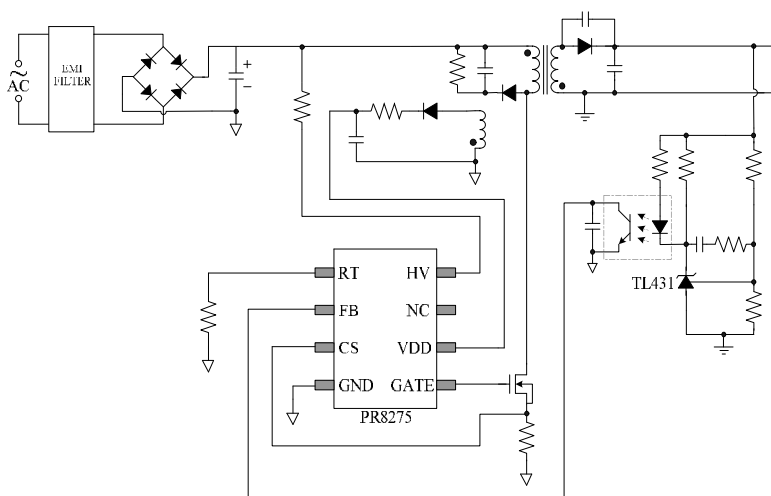


Fig.1

Pin Descriptions

PIN	NAME	FUNCTION
1	RT	This pin is to program the switching frequency. By connecting a resistor to ground to set the switching frequency.
2	FB	Voltage feedback pin (same as the FB pin in UC384X), By connecting a photo-coupler to close the control loop and achieve the regulation.
3	CS	Current sense pin, connect to sense the MOSFET current
4	GND	Ground
5	GATE	Gate drive output to drive the external MOSFET
6	VDD	Supply voltage pin
7	NC	Unconnected Pin
8	HV	Connect this pin to positive terminal of bulk capacitor to provide the startup current for the controller. When VDD voltage trips the UVLO(on), this HV loop will be off to save the power loss on the startup circuit.

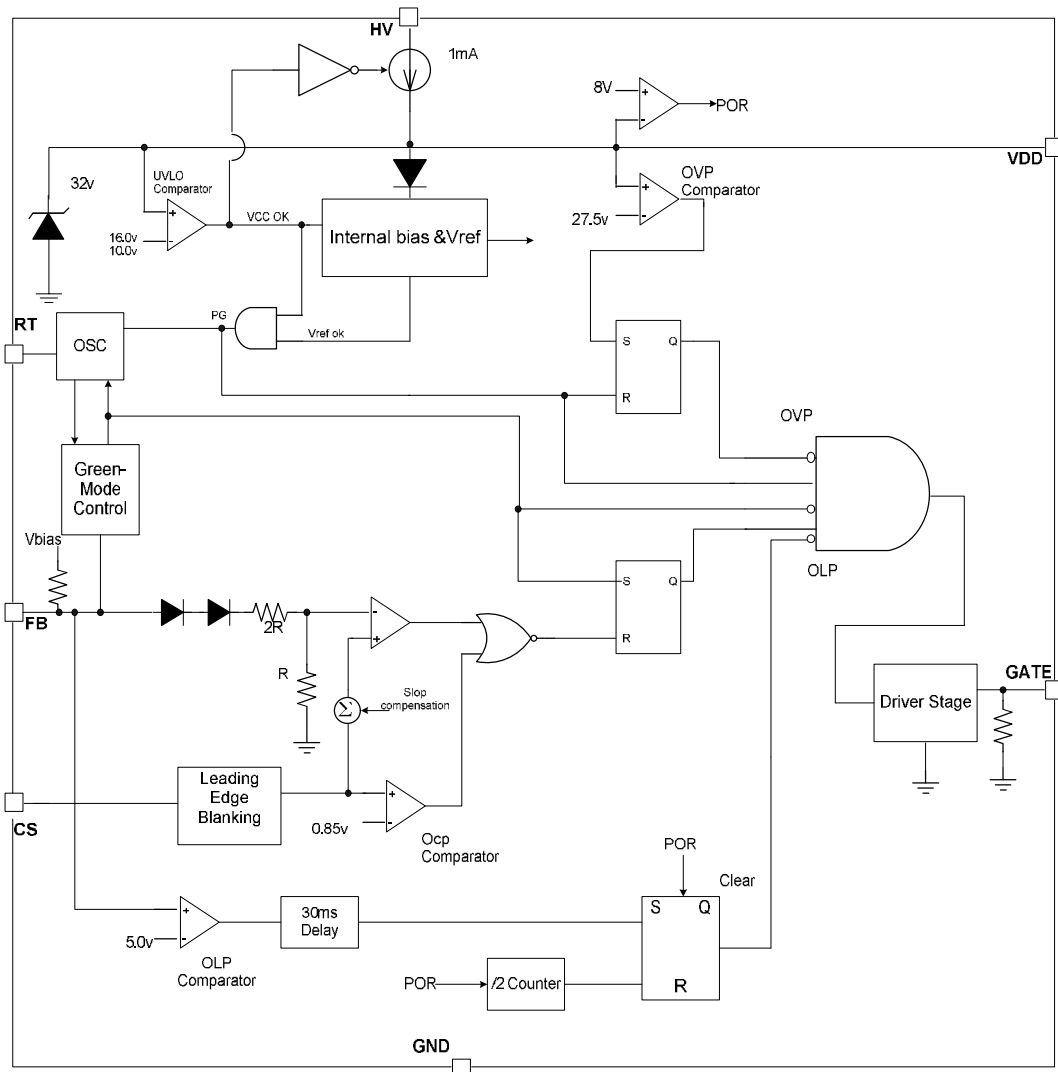


Fig.2

Absolute Maximum Ratings

Supply Voltage VDD	-30V
High-Voltage Pin, HV	-0.3V~500V
FB, RT, CS	-0.3 ~7V
Junction Temperature	150°C
Operating Ambient Temperature	-40°C to 85°C
Storage Temperature Range	-65°C to 150°C
Package Thermal Resistance (SOP-8)	160°C/W
Package Thermal Resistance (DIP-8)	100°C/W
Power Dissipation (SOP-8, at Ambient Temperature = 85°C)	400mW
Power Dissipation (DIP-8, at Ambient Temperature = 85°C)	650mW
Lead temperature (Soldering, 10sec)	260°C
Gate Output Current	500mA

Caution:

Stresses beyond the ratings specified in “Absolute Maximum Ratings” may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

Recommended Operating Conditions

Item	Min.	Max.	Unit
Supply Voltage VDD	11	25	V
VDD Capacitor	10	47	μ F
Switching Frequency	50	130	KHz

Electrical Characteristics(T_A = +25°C unless otherwise stated, VDD = 15.0V)

PARAMETER	PARAMETER CONDITIONS	MIN	TYP	MAX	UNITS
High-Voltage Supply (HV Pin)					
High-Voltage Current Source	VDD < UVLO(on), HV=500V	0.5	1.0	1.5	mA
Off-State Leakage Current	VDD > UVLO(off), HV=500V			35	μA
Supply Voltage (VDD Pin)					
Startup Current				100	μA
Operating Current (with 1nF load on GATE pin)	VFB=0V		2.0	3.0	mA
	VFB=3V		2.5	4.0	mA
	Protection tripped (OLP, OVP)		0.5		mA
UVLO (off)		9.0	10.0	11.0	V
UVLO (on)		15.0	16.0	17.0	V
OVP Level		25.0	27.5	30.0	V
Voltage Feedback (FB Pin)					
Short Circuit Current	VFB=0V		1.5	2.2	mA
Open Loop Voltage	FB pin open		6.0		V
Green Mode Threshold VFB			2.35		V
Current Sensing (CS Pin)					
Maximum Input Voltage		0.80	0.85	0.90	V
Leading Edge Blanking Time			350		nS
Input impedance		1			MΩ
Delay to Output			100		nS
Oscillator (RT pin)					
Frequency	RT=100KΩ	60.0	65.0	70.0	KHz
Green Mode Frequency	Fs=65.0KHz		20		KHz
Temp. Stability	(-40°C ~105°C)			3	%
Voltage Stability	(VDD =11V-25V)			1	%
Gate Drive Output (GATE Pin)					
Output Low Level	VDD =15V, Io=20mA			1	V
Output High Level	VDD =15V, Io=20mA	9			V
Rising Time	Load Capacitance=1000pF		50	160	nS
Falling Time	Load Capacitance=1000pF		30	60	nS
OLP (Over Load Protection)					
OLP Trip Level			5.0		V
OLP Delay Time (note)	Fs=65KHz		30		mS

Note: The OLP delay time is proportional to the period of switching cycle. So that, the lower RT value will set the higher switching frequency and the shorter OLP delay time.

Application Information

Operation Overview

As long as the green power requirement becomes a trend and the power saving is getting more and more important for the switching power supplies and switching adaptors, the traditional PWM controllers are not able to support such new

requirements. Furthermore, the cost and size limitation force the PWM controllers need to be powerful to integrate more functions to reduce the external part counts.

Internal High Voltage start up and UVLO

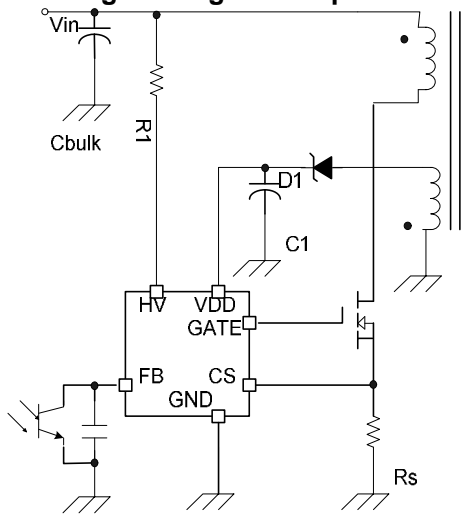


Fig.3

Traditional circuit powers up the PWM controller through a startup resistor to provide the startup current. However, the startup resistor consumes significant power which is more and more critical whenever the power saving requirement is coming tight. Theoretically, this startup resistor can be very high resistance value. However, higher resistor value will cause longer startup time. To achieve an optimized topology, as shown in figure 3, PR8275 implements a high-voltage startup circuit for such requirement. During the startup, a high-voltage current source sinks current from the bulk capacitor to provide the startup current as well as charge the VDD capacitor C1. During the startup transient, the VDD is lower than the UVLO threshold

thus the current source is on to supply a current with 1mA. Meanwhile, the VDD supply current is as low as 100µA thus most of the HV current is utilized to charge the VDD capacitor. By using such configuration, the turn-on delay time will be almost same no matter under low-line or high-line conditions. Whenever the VDD voltage is higher than UVLO(on) to power on the PR8275 and further to deliver the gate drive signal, the high-voltage current source is off and the supply current is provided from the auxiliary winding of the transformer. Therefore, the power losses on the startup circuit can be eliminated and the power saving can be easily achieved.

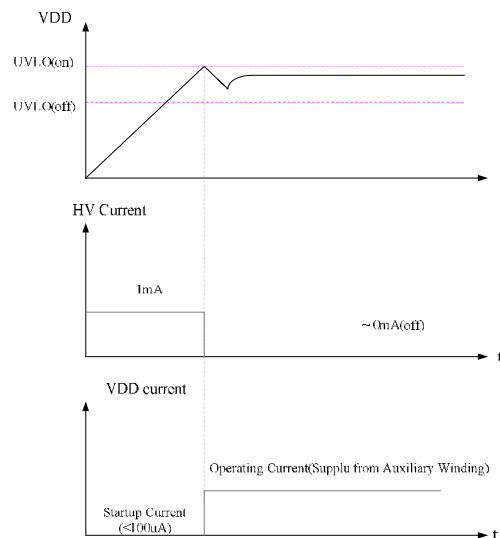


Fig.4

An UVLO comparator is included to detect

the voltage on the VDD pin to ensure the supply voltage enough to power on the PR8275 PWM controller and in addition to drive the power MOSFET. As shown in Fig.

Current Sensing, Leading-edge Blanking and the Negative Spike on CS Pin

The typical current mode PWM controller feedbacks both current signal and voltage signal to close the control loop and achieve regulation. The PR8275 detects the primary MOSFET current from the CS pin, which is not only for the peak current mode control but also for the pulse-by-pulse current limit. The maximum voltage threshold of the current sensing pin is set as 0.85V. Thus the MOSFET peak current can be calculated as:

$$I_{peak}(\text{max.}) = \frac{0.85}{R_s}$$

A 350ns leading-edge blanking (LEB) time is included in the input of CS pin to prevent the false-trigger caused by the current spike. In the low power application, if the total pulse width of the turn-on spikes is less than 350ns and the negative spike on the CS pin is not exceed -0.3V, the R-C filter (as shown in figure 5) can be eliminated. However, the total pulse width of the turn-on spike is related to the output power, circuit design and PCB layout. It is strongly recommended to add the small R-C filter (as shown in figure 6) for higher power application to avoid the CS pin damaged by the negative turn-on spike.

Output Stage and Maximum Duty-Cycle

An output stage of a CMOS buffer, with typical 500mA driving capability, is incorporated to drive a power MOSFET

Voltage Feedback Loop

The voltage feedback signal is provided from the TL431 in the secondary side through the photo-coupler to the FB pin of

4, a hysteresis is provided to prevent the shutdown from the voltage dip during startup. The turn-on and turn-off threshold level are set at 16V and 10.0V, respectively.

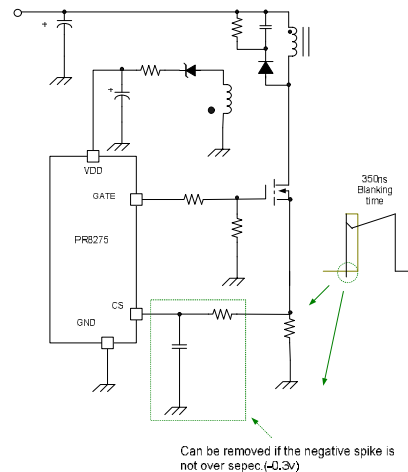


Fig.5

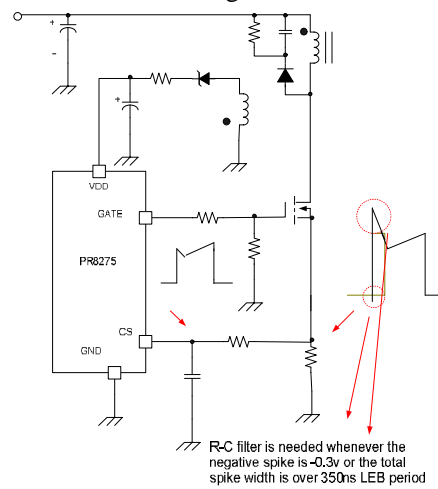


Fig.6

directly. And the maximum duty-cycle of PR8275 is limited to 75% to avoid the transformer saturation.

PR8275. The input stage of PR8275 with 2 diodes voltage offset then feeding into the voltage divider with 1/3 ratio, that is,

$$V_+ = \frac{1}{3}(V_{comp} - 2V_f)$$

A pull-high resistor is embedded internally thus can be eliminated on the external

Oscillator and Switching Frequency

Connecting a resistor from RT pin to GND according to the equation can program the normal switching frequency:

$$f_{sw} = \frac{65}{R_r(K\Omega)} \cdot 100(KHz)$$

Internal Slope Compensation

A fundamental issue of current mode control is the stability problem when its duty-cycle is operated more than 50%. To stabilize the control loop, the slope compensation is needed in the traditional UC384X design by injecting the ramp

On/Off Control

The PR8275 can be controlled to turn off by pulling FB pin to lower than 1.2V. The gate output pin of PR8275 will be disabled

Dual-Oscillator Green-Mode Operation

There are many difference topologies has been implemented in different chips for the green-mode or power saving requirements such as “burst-mode control”, “skipping-cycle Mode”, “variable off-time control “...etc. The basic operation theory

Over Load Protection (OLP)

To protect the circuit from the damage during over load condition or short condition, a smart OLP function is implemented in the PR8275. Figure 7 shows the waveforms of the OLP operation. Under such fault condition, the feedback system will force the voltage loop toward the saturation and thus pull the voltage on FB pin (V_{FB}) to high. Whenever the V_{FB} trips the OLP threshold 5.0V and keeps longer than 30mS (when switching

circuit.

The suggested operating frequency range of PR8275 is within 50KHz to 130KHz.

signal from the RT/CT pin through a coupling capacitor. In PR8275, the internal slope compensation circuit has been implemented to simplify the external circuit design.

immediately under such condition. The off mode can be released when the pull-low signal is removed.

of all these approaches intended to reduce the switching cycles under light-load or no-load condition either by skipping some switching pulses or reduce the switching frequency.

frequency is 65KHz), the protection is activated and then turns off the gate output to stop the switching of power circuit. The 30mS delay time is to prevent the false trigger from the power-on and turn-off transient. A divide-2 counter is implemented to reduce the average power under OLP behavior. Whenever OLP is activated, the output is latched off and the divide-2 counter starts to count the number of UVLO(off). The

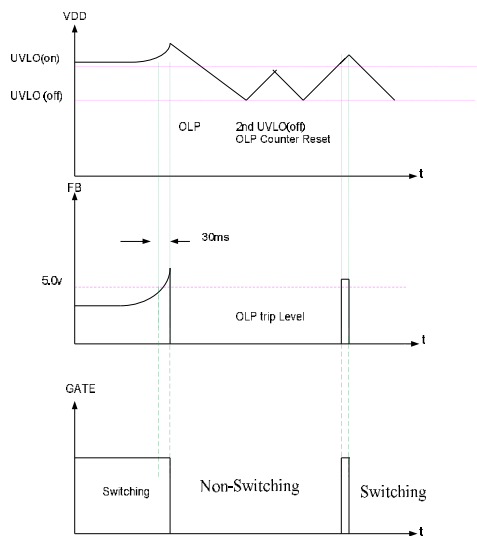


Fig.7

latch is released if the 2nd UVLO(off) point is counted then the output is recovery to

OVP (Over Voltage Protection) on VDD

The Vgs ratings of the nowadays power MOSFETs are most with maximum 30V. To prevent the Vgs from the fault condition, PR8275 is implemented an OVP function on VDD. Whenever the VDD voltage is higher than the OVP threshold voltage, the output gate drive circuit will be shutdown simultaneous thus to stop the switching of the power MOSFET until the next UVLO(on).

The VDD OVP function in PR8275 is an auto-recovery type protection. If the OVP condition, usually caused by the feedback loop opened, is not released, the VDD will tripped the OVP level again and re-shutdown the output. The VDD is

Fault Protection

A lot of protection features have been implemented in the PR8275 to prevent the power supply or adapter from being damaged caused by single fault condition on the open or short condition on the pin of PR8275. Under the conditions listed below,

switching again. By using such protection mechanism, the average input power can be reduced to very low level so that the component temperature and stress can be controlled within the safe operating area.

working as a hiccup mode. Figure 8 shows its operation. On the other hand, if the OVP condition is removed, the VDD level will get back to normal level and the output is automatically returned to the normal operation.

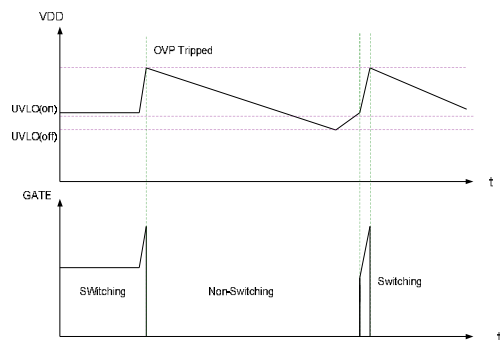


Fig.8

the gate output will be off immediately to protect the power circuit ---

1. RT pin short to ground
2. RT pin floating
3. CS pin floating

Pull-Low Resistor on the Gate Pin of MOSFET

In PR8275, an anti-floating resistor is implemented on the GATE pin to prevent the output from any uncertain state which may causes the MOSFET working abnormally or false triggered-on. However, such design won't cover the condition of disconnection of gate resistor R_g thus it is still strongly recommended to have a resistor connected on the MOSFET gate terminal (as shown in figure 9) to provide extra protection for fault condition.

This external pull-low resistor is to prevent the MOSFET from damage during power-on under the gate resistor is disconnected. In such single-fault condition, as show in figure 21, the resistor R8 can provide a discharge path to avoid the MOSFET from being false-triggered by the current through the gate-to-drain capacitor C_{gd} . Therefore, the MOSFET is

always pull-low and kept in the off-state whenever the gate resistor is disconnected or opened in any case.

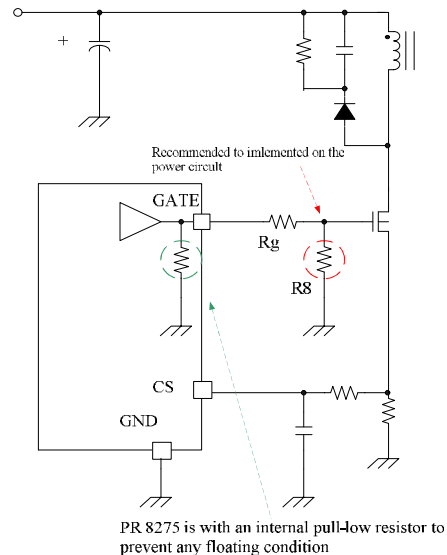


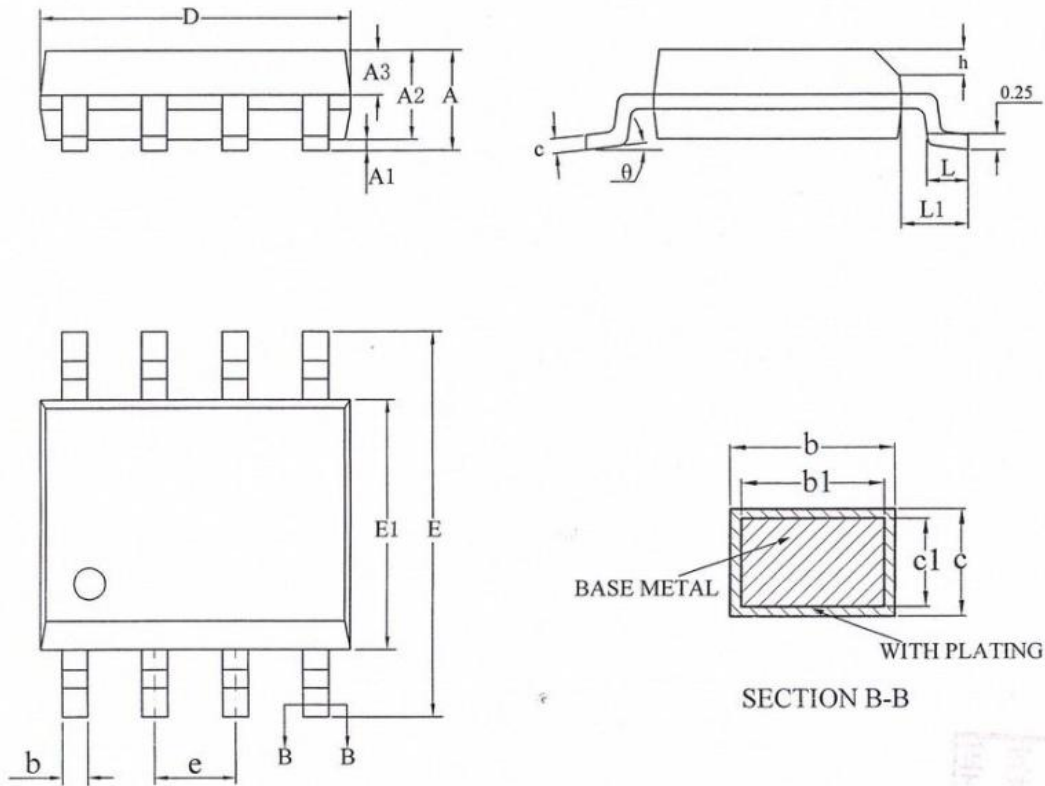
Fig.9

Protection Resistor on the Hi-V Path

In some other Hi-V process and design, there may cause a parasitic SCR between HV pin, VDD and GND. a small negative spike on the HV pin may trigger this parasitic SCR and causes the latch up between VDD and GND. And such latch up is easy to damage the chip because of the equivalent short-circuit which is

induced by such latch up behavior. So that PR8275 is with higher capability to sustain negative voltage than similar products. However, a $10K \Omega$ resistor is recommended to implement on the Hi-V path to be played the role as a current limit resistor whenever a negative voltage is applied in any case

SOP-8L



Dimensions

Symbol	Millimeter		
	Min.	Nom.	Max.
A	---	---	1.75
A1	0.10	---	0.225
A2	1.30	1.40	1.50
A3	0.60	0.65	0.70
b	0.39	---	0.48
b1	0.38	0.41	0.43
c	0.21	---	0.26
c1	0.19	0.20	0.21
D	4.70	4.90	5.10
E	5.80	6.00	6.20
E1	3.70	3.90	4.10
e	1.27BSC		
h	0.25	---	0.50
L	0.50	---	0.80
L1	1.05BSC		
θ°	0°	---	8°